

# Metalorganic chemical vapor deposition of InGaAsN using dilute nitrogen trifluoride

S.F. Cheng<sup>a</sup>, R.L. Woo<sup>a</sup>, A.M. Noori<sup>b</sup>, G. Malouf<sup>b</sup>, M.S. Goorsky<sup>b</sup>, R.F. Hicks<sup>a,\*</sup>

<sup>a</sup>Department of Chemical Engineering, University of California, Los Angeles, CA 90095, USA

<sup>b</sup>Department of Materials Science and Engineering, University of California, Los Angeles, CA 90095, USA

Received 11 May 2006; received in revised form 1 November 2006; accepted 8 November 2006

Communicated by R. Bhat

Available online 26 January 2007

## Abstract

The metalorganic chemical vapor deposition of  $\text{In}_{0.06}\text{Ga}_{0.94}\text{As}_{1-x}\text{N}_x$ , with  $x = 0.00\text{--}0.02$ , has been examined using nitrogen trifluoride ( $\text{NF}_3$ ) and tertiarybutylarsine. The solid N/V ratio increased linearly with the gas-phase N/V ratio up to a limit of 2.0% nitrogen in the film at a gas N/V = 0.35. No further increase in nitrogen content could be achieved at a growth temperature of 550 °C unless the feed rate of the group III sources was reduced. It was shown that  $\text{NF}_3$  addition to the reactor results in a growth rate decrease of 40% with increasing  $\text{NF}_3$  feed rate up to  $3.0 \times 10^{-4}$  mol/min (N/V = 0.35). Further addition of  $\text{NF}_3$  did not affect the growth rate, but caused the surface roughness to rise rapidly from 0.1 to over 1.0 nm. Results presented in this paper indicate that the increased surface roughness may be due to fluorine etching of the adsorbed group III elements.

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PACS: 81.05.Ea; 81.15.Gh; 68.47.Fg

Keywords: A3. Metalorganic chemical vapor deposition; B1. Nitrides

## 1. Introduction

Dilute III–V nitrides have been the focus of much research as the addition of a small amount of nitrogen into InGaAs can dramatically reduce the semiconductor's band gap [1,2]. An InGaAsN alloy with N concentrations in the range of a few percent is of interest for producing long-wavelength photodetectors, laser diodes, and vertical-cavity surface-emitting lasers (VCSELS) on GaAs substrates [3–5]. However, incorporating greater than 1.0% nitrogen in the film is difficult, especially for alloys grown by metalorganic chemical vapor deposition (MOCVD) [6]. In this case, extremely high ratios of dimethylhydrazine (DMH) to arsine must be fed to the reactor. Furthermore, the addition of indium greatly reduces the incorporation rate of nitrogen using DMH, making it harder to control the

InGaAsN composition during MOCVD [7,8]. This has led crystal growers to study other nitrogen precursors such as hydrazine [8], ammonia [9], tertiarybutylhydrazine [10,11], and nitrogen trifluoride [8,12].

$\text{NF}_3$  is a promising source of nitrogen for InGaAsN, since it exhibits high incorporation efficiency and is not affected by the presence of indium [8]. However,  $\text{NF}_3$  is a strong oxidizer that presents an explosion hazard when used in the hydrogen ambient found in MOCVD reactors [13]. Moreover, the use of pure  $\text{NF}_3$  has been found to result in a relatively narrow operating window for the InGaAsN growth process [8].

In this report, we assess the feasibility of using helium-diluted  $\text{NF}_3$  as a nitrogen source for the MOCVD of InGaAsN. Diluting the precursor in He allows one to keep the  $\text{NF}_3$  concentration in hydrogen below the flammability limit at the point of mixing [14].  $\text{NF}_3$  is found to incorporate nitrogen readily at feed rates below  $3.0 \times 10^{-4}$  mol/min, but at higher feed rates, increases the

\*Corresponding author. Tel.: +1 310 206 6865; fax: +1 310 206 4107.

E-mail address: [rhicks@ucla.edu](mailto:rhicks@ucla.edu) (R.F. Hicks).

surface roughness dramatically. The results presented below suggest that this may be due to fluorine etching of the group III elements.

## 2. Experimental methods

Indium gallium arsenide nitride films were grown on vicinal GaAs (001) substrates in a Veeco (formerly Emcore) D125 MOCVD reactor. The reactor was maintained at 60 Torr with a total flow of 37.0 standard-liter/min ultrahigh-purity hydrogen. The  $H_2$  was passed through a SAES Pure Gas, Inc. purifier (model PS4-MT3-H) which removed any remaining oxygen, nitrogen or carbon species to below a few parts per billion. The precursors were liquid trimethylindium (TMIn), trimethylgallium (TMGa), tertiarybutylarsine (TBAs), tertiarybutylphosphine (TBP), and 10%  $NF_3$  diluted in helium. Two separate InGaAsN structures were grown: 500-nm InGaAsN on a 50-nm InGaP etch-stop for growth rate determination; and 120-nm InGaAsN on a GaAs buffer for structural and compositional analysis. The GaAs and InGaP layers were deposited at 650 °C, while the InGaAsN layers were grown at 550 °C. The surface temperature was monitored in real-time using the emissivity-corrected RealTemp<sup>®</sup> instrumentation available from Veeco. After growth of the InGaAsN layer, the samples were cooled to room temperature and examined by in situ X-ray photoemission spectroscopy (XPS), and ex situ high-resolution X-ray diffraction (XRD) and atomic force microscopy (AFM). For the in situ measurements, the samples were transferred from the MOCVD reactor to the ultrahigh vacuum (UHV) surface analysis system via an interface chamber that was evacuated to  $1 \times 10^{-9}$  Torr.

Growth rates were determined by etching the InGaAsN up to the InGaP layer with an ammonium hydroxide/hydrogen peroxide/water solution in a 1:1:20 ratio, and then measuring the thickness of the film with a Dektak 8 profilometer. Core level photoemission spectra of the In 3d, Ga 2p, As 3d, and N 1s lines were collected using a PHI 3057 XPS spectrometer, with magnesium  $K_{\alpha}$  X-rays ( $h\nu = 1253.6$  eV). All spectra were taken in small area mode with a 7° acceptance angle and 23.5 eV pass energy. The take-off angle with respect to the surface normal was 25°. The surface composition was determined from the integrated intensity of the In 3d, Ga 2p, As 3d, and N 1s photoemission peaks, dividing by their sensitivity factors, 4.36, 3.72, 0.68 and 0.48, respectively. The N/V (In/III) ratio was obtained by dividing the N (In) atom% by the total group V (group III) atom%. The XRD measurements were made on a Bede D<sup>3</sup> high-resolution diffractometer using Cu  $K_{\alpha}$  X-rays. Atomic force micrographs were obtained on a Quesant 250 microscopy system in tapping mode. Film compositions were determined from room temperature photoluminescence (PL) and XRD using Vegard's law and Moon's method [15] in conjunction with bowing parameters available from Ferhat [16].

## 3. Results

### 3.1. MOCVD growth

Shown in Fig. 1 is the gas phase versus solid N/V ratios for InGaAsN films deposited at 550 °C on GaAs. Data from Kurtz et al. [8] have been included for reference. The films were grown at 3.4  $\mu\text{m}/\text{h}$ . A slightly higher gas phase N/V ratio was required to achieve the same solid composition as Kurtz obtained due to the better cracking efficiency of the TBAs used in the present work. The half-filled circle corresponds to a growth rate of 2.7  $\mu\text{m}/\text{h}$ , whereas the filled circle corresponds to 2.3  $\mu\text{m}/\text{h}$ . A linear relationship is observed between the solid N/V ratio and the gas N/V ratio up to 2.0% in the solid. Beyond this value, the solid N/V ratio could not be increased by raising the gas N/V ratio further. Instead one had to simultaneously raise the gas N/V ratio and lower the feed rate of the group III sources (i.e., the half-filled and filled circles).

Shown in Fig. 2 is the InGaAsN lattice mismatch relative to GaAs measured by XRD as a function of the TMGa and  $NF_3$  feed rates. All films in this figure have an indium content of  $5.8 \pm 0.2\%$ . At a TMGa feed rate of  $1.4 \times 10^{-4}$  mol/min, the epilayer peak shifts closer to the lattice matched condition with increasing  $NF_3$  feed rate up to  $3.0 \times 10^{-4}$  mol/min. However, above this value, the epilayer remains 0.1% mismatched independent of the  $NF_3$  feed rate. Improved lattice matching due to higher nitrogen incorporation was accomplished only when the TMGa and TMIn feed rates were decreased, while keeping the  $NF_3$  feed rate at  $2.7 \times 10^{-4}$  mol/min (cf. triangle and open box in Fig. 2).

The epilayer growth rate was found to decrease with increasing  $NF_3$  feed rate to the reactor. Shown in Fig. 3 is

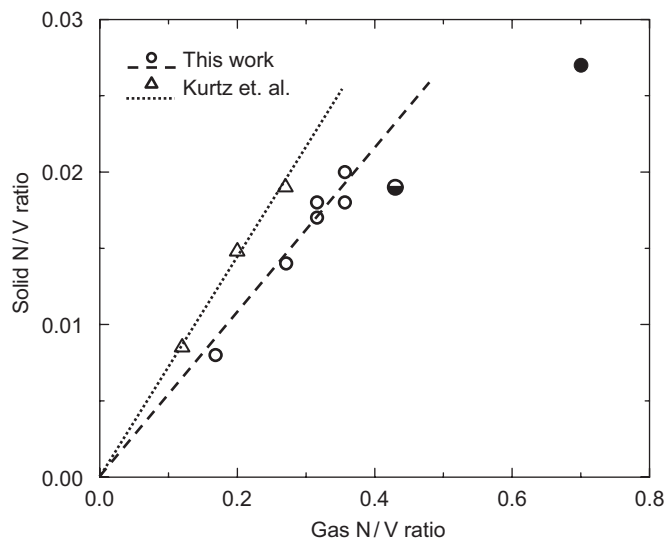


Fig. 1. Gas phase to solid N/V ratios for InGaAsN films deposited at 550 °C, including data from Kurtz et al. [8]. The TMGa flow rate for open circles was  $1.4 \times 10^{-4}$  mol/min, half-filled circle was  $1.0 \times 10^{-4}$  mol/min, and filled circle was  $8.8 \times 10^{-5}$  mol/min.

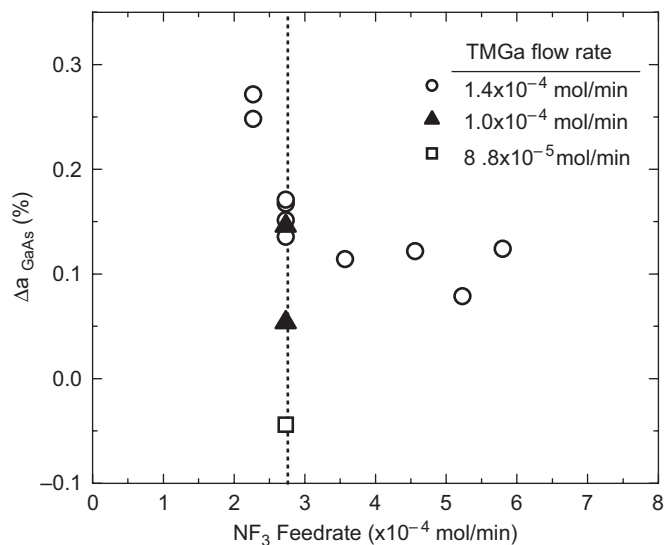


Fig. 2. Lattice mismatch of InGaAsN relative to GaAs as a function of  $\text{NF}_3$  feed rate. The gas phase TMGa/TMIn ratio was 28.0 for all TMGa flows listed in the legend.

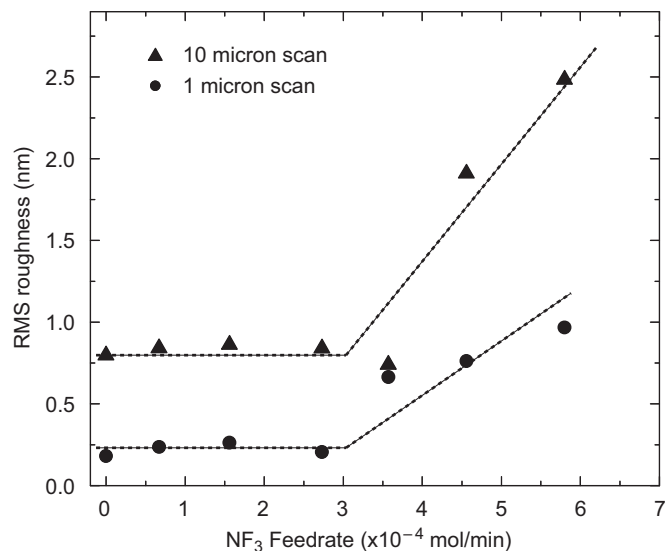


Fig. 4. Root-mean-square roughness as a function of  $\text{NF}_3$  feed rate for  $1 \times 1$  and  $10 \times 10 \mu\text{m}^2$  areas of the film surface. Films were grown at a TMGa feed rate of  $1.4 \times 10^{-4}$  mol/min.

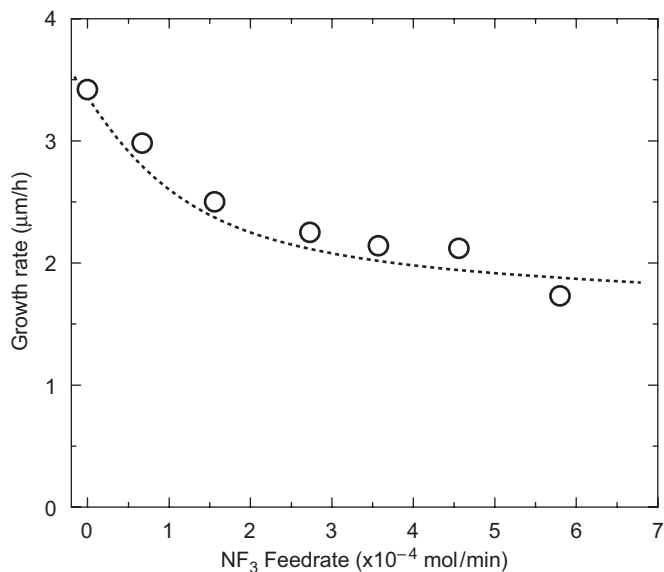


Fig. 3. Growth rate of InGaAsN films as a function of  $\text{NF}_3$  feed rate.

the growth rate as a function of the  $\text{NF}_3$  flow rate at a constant TMGa flow rate of  $1.4 \times 10^{-4}$  mol/min. The data points were produced from a series of measurements made on at least three samples grown at each condition. Upon addition of  $\text{NF}_3$  to the reactor, the growth rate drops quickly then levels off at about  $2.0 \mu\text{m}/\text{h}$  with increasing  $\text{NF}_3$  flow rate. At the stage where the growth rate levels off,  $\sim 3.0 \times 10^{-4}$  mol/min  $\text{NF}_3$ , an abrupt increase in the surface roughness of the film is observed. Shown in Fig. 4 is the measured root-mean-square (RMS) roughness on 1- and 10-micron areas as a function of the  $\text{NF}_3$  feed rate. The surface remains atomically flat with an average roughness of 0.2 nm (0.8 nm) over  $1.0$  ( $10.0$ )  $\mu\text{m}^2$  for  $\text{NF}_3$

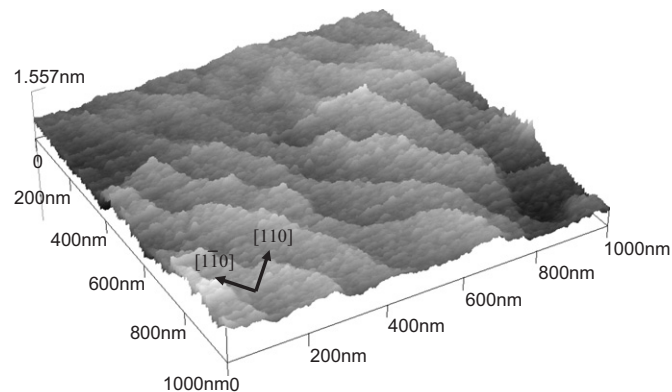


Fig. 5. AFM image of the surface of an InGaAsN film grown at TMGa and  $\text{NF}_3$  feed rates of  $1.4 \times 10^{-4}$  and  $2.7 \times 10^{-4}$  mol/min, respectively. Image size:  $1.0 \times 1.0 \mu\text{m}^2$ .

flows up to  $3.0 \times 10^{-4}$  mol/min. Increasing the  $\text{NF}_3$  flow to  $6.0 \times 10^{-4}$  mol/min causes the surface roughness to jump from 0.2 to 1.0 nm over  $1.0 \mu\text{m}^2$ . A similar increase is observed for the AFM measurement at  $10.0 \mu\text{m}^2$ .

A three-dimensional AFM image of a 120-nm-thick InGaAsN film grown at an  $\text{NF}_3$  feed rate of  $2.7 \times 10^{-4}$  mol/min and  $550^\circ\text{C}$  is presented in Fig. 5. Atomically smooth terraces are observed with a terrace height of 0.3 nm. Conversely, when one increases the  $\text{NF}_3$  feed to the reactor to  $3.6 \times 10^{-4}$  mol/min, the surface roughens from 0.2 to 0.7 nm over an area of  $1.0 \mu\text{m}^2$ . One might think that this is due to strain induced by the higher nitrogen content in the film. However, because the film is under compression, the incorporation of additional nitrogen into the film should reduce the total strain. Therefore, we surmise that the increased roughness originates from a chemical process at the surface.

### 3.2. Annealing in $\text{NF}_3$

In order to gain more insight into the processes occurring at the surface of InGaAsN films during growth,  $\text{NF}_3$  vacuum annealing studies were carried out. Duplicates of the film used to produce the image in Fig. 5 were grown and transferred to the UHV system through an interface chamber with a base pressure of  $1 \times 10^{-9}$  Torr without exposure to air. They were then annealed for 20 min each at 180, 310, 420, 510 and 530 °C in  $1 \times 10^{-6}$  Torr  $\text{NF}_3$ . Confirmation of  $\text{NF}_3$ -induced roughening of the InGaAsN surface is shown in Fig. 6. The  $\text{NF}_3$  treatment caused the surface to become severely pitted, with a pit density of  $1.85 \times 10^8 \text{ cm}^{-2}$ . These features are elongated in the [110] direction and have an average width and depth of 40.0 by 1.0 nm, respectively.

The InGaAsN samples were examined in situ by X-ray photoemission spectroscopy prior to AFM characterization. Shown in Table 1 are the surface atomic compositions, N/V and In/III ratios, and RMS roughness recorded for the freshly grown (Fig. 5),  $\text{NF}_3$ -annealed (Fig. 6), and a vacuum-annealed control sample. After the InGaAsN film was annealed in  $\text{NF}_3$  at 530 °C, the ratio of the indium to group III concentration increased by about threefold. This may be compared to the sample annealed in vacuum, where the In/III ratio remained constant. At the same time, there is no significant change in the N/V ratio in either of the annealed samples. The concentration of fluorine measured by XPS is below the detection limit for the as-grown and vacuum-annealed samples and is 2.0% after annealing in  $\text{NF}_3$ . The ex situ AFM measured RMS roughness increases

more noticeably when annealed in  $\text{NF}_3$  compared to in vacuum, increasing the surface roughness of the as-grown film from 0.18 to 0.33 and 0.21 nm, respectively.

X-ray diffraction and PL measurements revealed that changes in the bulk composition of the film occurred after annealing the sample in  $1 \times 10^{-6}$  Torr of  $\text{NF}_3$  at 530 °C [17]. It was found that annealing for 1 h caused the bulk nitrogen to increase a lot, from 1.1 to 1.7 mol%, whereas the bulk indium increased slightly, from 5.5 to 5.7 mol%. These findings will be detailed in a separate report [17].

### 4. Discussion

The incorporation efficiency of nitrogen into InGaAsN using helium-diluted nitrogen trifluoride and tertiarybutylarsine is comparable to that obtained by MOCVD with pure  $\text{NF}_3$  and  $\text{AsH}_3$  [8]. In the former case, a slightly higher N/V ratio in the feed is needed to achieve the same solid composition [8]. As can be seen in Fig. 1, the N/V ratio in the film increases linearly with the N/V ratio in the feed up to a value of 0.02. After that, further increases in the  $\text{NF}_3$  feed ratio have no effect on the solid composition (cf. Fig. 2). At a growth temperature of 550 °C, we were only able to raise the nitrogen in the alloy further by decreasing the feed rate of TMGa and TMIIn to the reactor.

The shift of the XRD peak towards GaAs at lower TMGa flow rates in Fig. 2 is attributed to increased nitrogen incorporation. A similar shift may be expected if indium incorporation were to decrease. However, we expect the In incorporation rate into the solid to be unaffected by the presence of  $\text{NF}_3$  during growth. An InGaAs calibration run was performed for the standard growth rate of 3.4  $\mu\text{m}/\text{h}$ . The XRD-measured In concentration for the InGaAs sample was identical to that estimated for the InGaAsN samples from the XRD and PL data. This is in agreement with Kurtz and coworkers [8], who have shown by secondary ion mass spectroscopy (SIMS) and electron probe microanalysis that the addition of nitrogen using  $\text{NF}_3$  does not change the amount of indium incorporated. PL measurements made on selected samples show a decrease in band gap that is consistent with nitrogen incorporation at a constant group III composition. For example, InGaAsN band gaps of 1.253, 1.250 and 1.211 were recorded for a lattice mismatch to GaAs of 0.17%, 0.14% and  $-0.04\%$ , respectively.

The results obtained in this study suggest that etching of the group III elements occurs on the film surface that

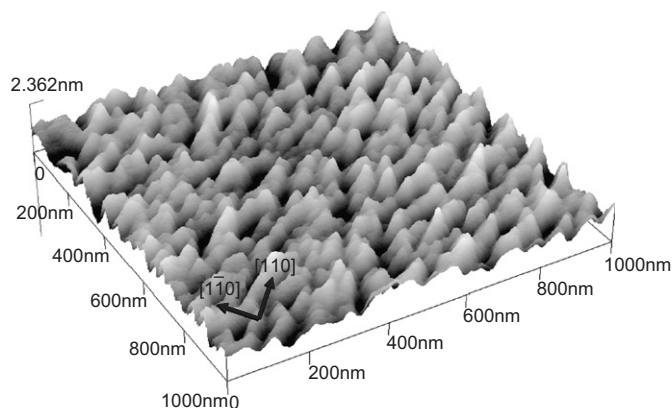


Fig. 6. AFM image of the surface in Fig. 5 after exposure to  $1.0 \times 10^{-6}$  Torr of  $\text{NF}_3$  at 180–510 °C. Image size:  $1.0 \times 1.0 \mu\text{m}^2$ .

Table 1  
Surface composition in atomic % for the as-grown and annealed InGaAsN films determined by X-ray photoemission

Annealing ambient	In	Ga	As	N	F	N/V	In/III	RMS roughness (nm)
As-grown	$2.3 \pm 0.5$	$29.7 \pm 1.6$	$57.5 \pm 2.1$	$9.8 \pm 1.4$	0.0	$0.15 \pm 0.03$	$0.07 \pm 0.01$	0.18
$\text{NF}_3$	$9.0 \pm 0.5$	$31.3 \pm 1.6$	$48.2 \pm 2.1$	$9.5 \pm 1.4$	$2.0 \pm 0.5$	$0.16 \pm 0.03$	$0.22 \pm 0.01$	0.33
Vacuum	$2.3 \pm 0.5$	$36.7 \pm 1.6$	$51.0 \pm 2.1$	$10.3 \pm 1.4$	0.0	$0.17 \pm 0.03$	$0.06 \pm 0.01$	0.21

competes with InGaAsN film growth. In particular, it can be seen in Fig. 3 that the growth rate declines from 3.5 to 2.0  $\mu\text{m}/\text{h}$  as the  $\text{NF}_3$  feed rate rises from 0.0 to  $3.0 \times 10^{-4}$  mol/min. At higher  $\text{NF}_3$  feed rates, the growth rate remains constant, but as shown in Fig. 4, there is an abrupt increase in the surface roughness. Further evidence for fluorine etching of adsorbed Ga and In is obtained upon annealing the InGaAsN film in  $1.0 \times 10^{-6}$  Torr of  $\text{NF}_3$  at 530 °C. The AFM image in Fig. 6 reveals that the surface has become severely pitted with an increase in roughness from 0.18 to 0.33 nm. The same anneal conducted in vacuum conditions resulted in an increase from 0.18 to 0.21 nm. We suspect that the interaction of the fluorine with the adsorbed group III elements decreases their diffusion length, leading to 3-D nucleation and island growth, instead of incorporation at step edges as they sweep across the surface. It may be that the etch rates of adsorbed Ga and In with fluorine are similar, such that their incorporation rates into the film are relatively unaffected.

Nonetheless, gas-phase reactions between  $\text{NF}_3$  and the group III metalorganic precursors cannot be ruled out, and can explain the observed drop in the film growth rate. Moreover, increased nitrogen incorporation from annealing in  $\text{NF}_3$  may increase local strain, resulting in phase separation and the observed undulations on the film surface as detailed in a separate report [17]. Clearly, more detailed studies of dilute nitride growth using  $\text{NF}_3$  must be carried out to fully elucidate the growth rate decrease and the possibility of fluorine-induced etching.

In conclusion,  $\text{NF}_3$  is an efficient source for incorporating up to 2.0% nitrogen into InGaAsN films grown by MOCVD. Beyond 2.0% nitrogen, it is difficult to achieve lattice matching to GaAs.

## Acknowledgment

Funding for this research was provided by the UC Discovery Program.

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